Printed Frequency Scanning Antenna Array with Wide Scanning Angle Range

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Abstract—Leaky-wave radiations are usually generated by leaking the electromagnetic energy gradually over a structure. By using the coupling effect and leaky-wave properties, this paper designs a novel 1-D frequency scanning antenna array. The antenna is intended for the direct imaging radar sensors. The simulated results show that the scanning angle can stay in the range from $-60^\circ$ to $30^\circ$. The proposed 1-D antenna array was manufactured, and the measured results are consistent with the simulated ones.

1. INTRODUCTION

Searching a low-cost means to measure the distance and angle of targets is always a great challenge in the commercial radar sensors researches [1–3, 11–18]. In recent years, with the attractive advantages such as low profile, compact structure, wide frequency band, frequency beam scanning characteristics and easiness of integration with planar circuits, scientists and researchers have paid much attention to planar leaky-wave antennas (LWAs) [2–10]. By leaking electromagnetic energy along the structure, the radiated beams of LWAs can scan in the space as frequency changes [2]. Frequency beam scanning antennas are widely used in radar and wireless communication systems [3–5, 19].

In this paper, the propagation properties of the element of leaky-wave antenna are analyzed. The proposed antenna is fabricated and measured. The simulated results indicate that this printed antenna exhibits a good scanning performance of $-60^\circ$ to $30^\circ$ with a maximum gain of 16.87 dBi, and the antenna has flat gain of more than simulated 13 dBi in the whole operation band from 8.3 GHz to 10.9 GHz. The measured results are consistent with simulated ones.

2. ELEMENT OF LEAKY-WAVE ANTENNA

In the antenna array design, the property of phase shifters is the main reason to realize beam scanning. In this paper, the phase adjustment is realized through the change of frequency. The proposed phase shifter is shown in Fig. 1. This phase shifter has dual functions: it can be used as phase shifter, and it can also leak electromagnetic waves and be used as radiating element. The increased coupling effect can contribute to increasing scanning angle. The proposed element has three layers. The top layer is a unit cell of LWAs. The middle layer is a substrate with permittivity of 2.65 and loss tangent of 0.001. The bottom layer is a metallic ground. The optimum dimensions are: $h = 1.5$ mm, $l = 26$ mm, $w = 16.35$ mm, $p = 1$ mm, $a = 0.5$ mm, $w_s = 0.75$ mm, $s_g = 0.04$ mm and $g = 0.35$ mm.
This phase shifter is simulated using HFSS, and its results are shown in Fig. 2. From Fig. 2, it can be seen that this element can radiate some electromagnetic power into space, and the phase shift from 8.3 GHz to 10.9 GHz is 215°.

3. ANTENNA DESIGN

Based on the radiation element, we design a linear scanning antenna array, as shown in Fig. 3. This proposed linear scanning antenna array can radiate EM waves into free space element by element gradually, and each element also has a different phase shift as frequency changes, thus this proposed antenna can realize beam scanning. Using Ansoft HFSS, we also simulate this proposed 1-D linear array antenna, and its results are shown in Fig. 4. As expected, the radiated beams of this linear array antenna can scan in the space as frequency changes, and its scanning angle can stay in the range from −60° to 30°.

In order to make a better understanding of the beam scanning performance, the radiated far-field patterns of the proposed antenna array at different frequencies under polar coordinate system are illustrated in Fig. 5.

As shown in Fig. 5, it can be seen that the main beam of the proposed antenna array can point at different directions of the free space as frequency varies.

In order to validate the correctness of the design in this paper, a sample corresponding to the simulated one is fabricated and tested. A antenna photograph and measurement environment are shown in Fig. 6. In order to prevent reflection of non-radiated power deteriorating the performance
Figure 3. Proposed 1-D linear antenna array.

Figure 4. Simulated relative radiation pattern for the linear antenna array in E-plane.

Figure 5. Radiated far-field patterns of the proposed antenna array at (a) 8.6 GHz, (b) 9 GHz, (c) 10 GHz and (d) 10.9 GHz.

of antenna array, a matching load is loaded at the end of the array in the measurement process. The simulated and measured reflection and transmission coefficients are shown in Fig. 7. It can be seen from Fig. 7 that the measured results are in good agreement with the simulated ones. The simulated and measured $S_{11}$ and $S_{21}$ are all less than $-7.3$ dB in the frequency band of 8.3–10.9 GHz. It indicates that more than 82% electromagnetic energy is radiated into free space by the antenna elements. The $S_{11}$ has a maximum of $-7.3$ dB around 10 GHz, mainly attributed to the mutual coupling between adjacent phase shifters.
Figure 6. Fabricated sample and measurement environment.

Figure 7. Simulated and measured (a) reflection coefficients ($S_{11}$) and (b) transmission coefficients ($S_{21}$) of proposed antenna array.

Figure 8. (a) Measured relative radiation pattern of the antenna array in $E$-plane and (b) simulated and measured gains for the antenna array in $E$-plane.
The antenna radiation patterns are measured in a chamber with a far-field setup from 8 GHz to 11 GHz. The antenna gain is measured using a standard horn antenna. Since we know the real gain of standard antenna, we first measure the proposed antenna’s gain and then measure the standard antenna’s gain in the same measurement environment. Compared with the standard horn antenna, we can get the gain of the proposed antenna. Fig. 8(a) shows the measured radiation patterns. It is indicated that the measured beam angle is scanned from $-62^\circ$ to $29^\circ$, which is consistent with simulated ones. From the simulated and measured results, it is proved that the wide angle scanning property is realized for the proposed antenna array. The simulated and measured gains of the antenna array are shown in Fig. 8(b). In the whole operating frequency band of 8.3–10.9 GHz, the simulated antenna gain varies between 12.95 and 16.87 dBi, and the measured antenna gain varies between 10.55 and 15.31 dBi. The measured results are in excellent agreement with the simulations.

In order to clarify the effectiveness the antenna array in this paper, some similar beam-scanning antennas reported in the references are compared with the proposed antenna array in Table 1. It can be concluded that the proposed antenna array in this paper has a significantly wide scanning angle.

Table 1. Comparison of the proposed antenna with some similar works reported in references.

<table>
<thead>
<tr>
<th>Antenna</th>
<th>Frequency range (GHz)</th>
<th>Scanning angle (degrees)</th>
</tr>
</thead>
<tbody>
<tr>
<td>[2]</td>
<td>8.5–9.8</td>
<td>18</td>
</tr>
<tr>
<td>[6]</td>
<td>8.9–9.5</td>
<td>12</td>
</tr>
<tr>
<td>[7]</td>
<td>5–11</td>
<td>55</td>
</tr>
<tr>
<td>[9]</td>
<td>8.9–10.6</td>
<td>73.5</td>
</tr>
<tr>
<td>This paper</td>
<td>8.3–10.9</td>
<td>90</td>
</tr>
</tbody>
</table>

4. CONCLUSION

In this paper, a novel phase shifter is designed. This phase shifter has dual functions. It can be used as a phase shifter and radiated element. Based on the proposed element, we design a 1-D linear antenna array with the ability of wide scanning angle. In the operating frequency band of 8.3–10.9 GHz, the simulated scanning angle of the antenna array can stay in the range from $-60^\circ$ to $30^\circ$, while the measured scanning angle is from $-62^\circ$ to $29^\circ$. The simulated gains of the antenna are more than 12.95 dBi, and the measured ones are more than 10.55 dBi. The measurements are in good agreement with simulations. Because of the wide beam-scanning ability, easiness of design and low cost in fabrication, the proposed antenna array has potential applications in radar and wireless communication systems.

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REFERENCES


