A Hybrid SAR Autofocus Technique by Two Methods of Sub-Aperture Estimation and Iterative Golden Section Search

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Abstract—In a real airborne synthetic aperture radar (SAR), its major phase errors are usually composed of two categories, such as slow-time varying phase errors (less than several cycles of change in phase during synthetic aperture time) and fast-time varying phase errors (otherwise, including wide band random) according to the motion of aircraft. If the fast errors are no more negligible compared to the slow errors, they should be estimated and then compensated accurately to obtain a well focused image. However, it is not proper to estimate all phase errors at the same time like conventional autofocus techniques because the estimation of the fast-time varying phase errors are seriously affected by blurring in image due to the slow-time varying phase errors. In this paper, we presents an accurate hybrid phase estimation technique using two independent estimation stages of sub-aperture and an iterative golden section search method, which has advantages over several existing methods, because of its better estimation accuracy and less sensitive to the quality of extracted range bins as well as requiring less computation time. The performance of our method is illustrated by simulations of point targets and an experiment with real SAR data.

1. INTRODUCTION

Autofocus techniques for synthetic aperture radar (SAR) have been a major concern, and many attempts have been made to improve their performance for real SAR applications. Autofocus techniques are generally categorized into two types according to the estimation method: parametric or non-parametric. In parametric methods [1,2] phase errors are approximated by an appropriate model with specific parameters, whereas non-parametric method [3–5] do not require a phase error model, thus allowing us to estimate a wide variety of phase errors. Non-parametric methods such as the phase gradient algorithm (PGA) [3,4], the eigenvector method (EVM) [6], the weighted least square (WLS) [7], and the successive parameter adjustment (SPA) [8] are widely used owing to their good performance compared to the computation time required. However, the performance of non-parametric methods, which require range bins for estimation, seriously depends on the quality of the extracted range bins from an unfocused image. Studies have been conducted on the selection of good range bins and on an iterative selection method during estimations [9, 10] to overcome the above constraint. Furthermore, if the fast-varying phase errors such as wideband random (WBR) phase errors are serious and should be removed for a well-focused image as often experienced in low-altitude airborne SAR, a gradient-based non-parametric method such as PGA is not proper to use for an accurate estimation because the calculations of gradient are severely affected by the WBR phase errors. The SPA method modeling unknown phase errors using orthogonal polynomial (Legendre) shows a good performance in case of the polynomial type of phase errors. However, it is not proper to apply in case of the WBR phase errors because it is insufficient to approximate the phase errors with finite polynomials. A non-gradient-based method [11] was proposed to cope with the WBR phase errors for inverse SAR (ISAR) applications; however, it requires a considerable

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amount of computation time for the case of SAR, which requires a much longer synthetic aperture time (SAT) than ISAR.

In this paper, we propose a hybrid estimation technique to provide an accurate estimation for both the slow-time varying (STV) errors and the WBR phase errors. It is assumed that the extracted range bin contains a dominant point like scatterer (target) with some strong clutters, similar to a real SAR environment. The proposed method consists of two estimation stages, the first for the estimation of STV phase errors and the second for the estimation of all errors, including any residual errors remaining after the first stage. A sub-aperture estimation method is utilized for the first stage, and then we adopt an iterative golden section search (IGSS) method for the second stage to ensure an efficient computation time while maintaining an accurate estimation. Simulations and an experiment with real SAR data illustrate the performance of our method.

2. FIRST STAGE: ESTIMATION OF THE STV PHASE ERRORS

2.1. Model of a Single Range Bin for Phase Estimation

The single range bin extracted from an unfocused image can be modeled as

$$g(t) = \left(a_0 e^{j\omega_0 t} + \sum_{c=1}^C a_c e^{j\omega_c t}\right) e^{j\varphi(t)}, \quad a_0 > a_c.$$

$$\tag{1}$$

Here, t indicates the azimuth time; C denotes the number of non-negligible clutters (NNCs) which cannot be neglected in comparison to the dominant target. Additionally, a_0 and a_c , and ω_c and ω_c are respectively the amplitudes and angular frequencies of the target and NNCs. The overall phase error is denoted as $\varphi(t)$, and it is simply assumed to have two types of errors, defined as $\varphi_L(t)$ for the STV phase error and $\varphi_R(t)$ for the WBR phase error (see Figure 1, for example). The purpose of the first stage of our method is to estimate $\varphi_L(t)$ in (1) and compensated it prior to proceeding to the second stage for an accurate estimation.

2.2. Estimation of the $\varphi_L(t)$ by Sub-Aperture Method

As in other sub-aperture methods [12], the SAT is divided into N non-overlapping segments (u_1, \ldots, u_N) , as shown in Figure 1. The *n*th segment phase error $\varphi_{L,n}(t)$ is modeled as

$$\varphi_{L,n}(t) = e^{j\phi_n(t,\boldsymbol{\beta}_n)}, \quad \phi_n(t,\boldsymbol{\beta}_n) = \sum_{q=0}^Q \beta_{n,q} t^q.$$
⁽²⁾

Here, Q indicates the polynomial order of the model, and β_n is the parameter to be estimated. We define $z(t) = e^{j \angle g(t)}$ by (1) with z_k being the sample of $z(t = t_k)$. All z_k values are assumed to have an equal length of M, and each segment thus has M datum pairs (t_i, z_i) with the expression of $\hat{z}_i = (\hat{x}_i, \hat{y}_i)$



Figure 1. An example of two types of phase error and segment configuration for sub-aperture estimations.

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as the estimation of $z_i = (x_i, y_i)$. The goal is to optimize the β_n parameters of the $\phi_n(t, \beta_n)$ model such that the sum of the squares of the error $E(\beta)$ is minimized (the subscript 'n' is omitted hereafter for simplicity):

$$E(\boldsymbol{\beta}) = \sum_{i=1}^{M} |z_i - \hat{z}_i|^2 = \sum_{i=1}^{M} \left| z_i - e^{j\phi(t_i,\boldsymbol{\beta})} \right| = \sum_{i=1}^{M} \left\{ [x_i - \cos\left(\phi\left(t_i,\boldsymbol{\beta}\right)\right)]^2 + [y_i - \sin\left(\phi\left(t_i,\boldsymbol{\beta}\right)\right)]^2 \right\}.$$
 (3)

The normal equation is obtained by a linearization of \hat{z}_i around the pre-estimated β^{l-1} via a Taylor series expansion of the first order, as follows:

$$\hat{x}_{i}\left(t_{i},\beta^{l}\right) \approx \hat{x}_{i}\left(t_{i},\beta^{l-1}\right) + \sum_{s=0}^{Q} \frac{\partial \hat{x}_{i}\left(t_{i},\beta^{l-1}\right)}{\partial \beta_{s}} \left(\beta_{s}^{l} - \beta_{s}^{l-1}\right) = \hat{x}_{i}\left(t_{i},\beta^{l-1}\right) + \sum_{s=0}^{Q} g_{is}\Delta\beta_{s}$$

$$\hat{y}_{i}\left(t_{i},\beta^{l}\right) \approx \hat{y}_{i}\left(t_{i},\beta^{l-1}\right) + \sum_{s=0}^{Q} \frac{\partial \hat{y}_{i}\left(t_{i},\beta^{l-1}\right)}{\partial \beta_{s}} \left(\beta_{s}^{l} - \beta_{s}^{l-1}\right) = \hat{y}_{i}\left(t_{i},\beta^{l-1}\right) + \sum_{s=0}^{Q} h_{is}\Delta\beta_{s}$$

$$\text{where } g_{is} = \frac{\partial \hat{x}_{i}}{\partial \beta_{s}}, \quad h_{is} = \frac{\partial \hat{y}_{i}}{\partial \beta_{s}}, \quad \Delta\beta_{s} = \beta_{s}^{l} - \beta_{s}^{l-1}.$$

$$(4)$$

Taking the gradient of (3) with respect to β_q , (q = 0, 1, 2) and using the relationships in (4) results in

$$\frac{\partial E\left(\boldsymbol{\beta}\right)}{\partial\beta_{q}} = \sum_{i=1}^{M} \left[\frac{\partial E\left(\boldsymbol{\beta}\right)}{\partial\hat{x}_{i}} \cdot \frac{\partial\hat{x}_{i}}{\partial\beta_{q}} + \frac{\partial E\left(\boldsymbol{\beta}\right)}{\partial\hat{y}_{i}} \cdot \frac{\partial\hat{y}_{i}}{\partial\beta_{q}} \right]$$
$$= 2\sum_{i=1}^{M} \left[\left(x_{i} - \hat{x}_{i} - \sum_{s=0}^{Q} g_{is}\Delta\beta_{s} \right) g_{iq} + \left(y_{i} - \hat{y}_{i} - \sum_{s=0}^{Q} h_{is}\Delta\beta_{s} \right) h_{iq} \right]$$
$$= 2\sum_{i=1}^{M} \left[\left(\Delta x_{i} - \sum_{s=0}^{Q} g_{is}\Delta\beta_{s} \right) g_{iq} + \left(\Delta y_{i} - \sum_{s=0}^{Q} h_{is}\Delta\beta_{s} \right) h_{iq} \right].$$
mal equation is obtained as

Then normal equation is obtained as

$$\sum_{i=1}^{M} \sum_{s=0}^{Q} (g_{is}g_{iq} + h_{is}h_{iq})\Delta\beta_s = \sum_{i=1}^{M} (\Delta x_i g_{iq} + \Delta y_i h_{iq}).$$
(5)

In vector notation, (5) becomes (here, T indicates transpose)

$$\left(\mathbf{G}^{\mathrm{T}}\mathbf{G} + \mathbf{H}^{\mathrm{T}}\mathbf{H}\right)\boldsymbol{\Delta}\boldsymbol{\beta} = \mathbf{G}^{\mathrm{T}}\boldsymbol{\Delta}\mathbf{x} + \mathbf{H}^{\mathrm{T}}\boldsymbol{\Delta}\mathbf{y}.$$

In this paper, the normal equation is solved by the LMA (Levenberg-Marquardt Algorithm) with the damping parameter λ [13] as

$$\left[\mathbf{G}^{\mathbf{T}}\mathbf{G} + \mathbf{H}^{\mathbf{T}}\mathbf{H} + \lambda \cdot \operatorname{diag}\left(\mathbf{G}^{\mathbf{T}}\mathbf{G} + \mathbf{H}^{\mathbf{T}}\mathbf{H}\right)\right] \mathbf{\Delta\beta} = \mathbf{G}^{\mathbf{T}}\mathbf{\Delta x} + \mathbf{H}^{\mathbf{T}}\mathbf{\Delta y}.$$
 (6)

2.3. Good Initial Guess of β_n

Like other iterative methods, a good initial guess of β^0 leads to a better optimal solution. When a quadratic model is used, a good β^0 can be determined by an efficient search strategy based on the following characteristics:

1) β_2 only dominates the entropy of the image; thus, β_2^0 is determined by a search for a value of β_2 that minimizes the entropy function defined below

$$H[\beta_2] = \sum_{k=0}^{M-1} |G(k,\beta_2)| \ln [|G(k,\beta_2)|],$$

$$G(k,\beta_2) = \sum_{m=0}^{M-1} z_m e^{-j\frac{2\pi km}{M}} e^{-j\beta_2 m^2}, \quad \beta_2^0 = \arg \min_{\beta_2} \{H[\beta_2]\}$$

2) β_1 causes a shift in the image domain according to the value of β_1 ; thus, β_1^0 is determined by measuring the amount of shift in $|G(k; \beta_2^0)|$.

3) β_0^0 is finally determined by a search for a value of β_0 that minimizes the error cost function with the previously determined initial estimates of β_2^0 and β_1^0 , as defined below

$$E(\beta_0; \beta_1^0, \beta_2^0) = \sum_{i=1}^M |z_i - \hat{z}_i|^2$$

$$\beta_0^0 = \arg\min_{\beta_0} \left\{ E\left(\beta_0; \beta_1^0, \beta_2^0\right) \right\}.$$

In our experiment, β_n was sufficiently obtained by solving (6) within dozens of iterations with feasible values of β^0 .

3. SECOND ESTIMATION STAGE FOR THE WBR PHASE ERRORS

After the compensation of $\varphi_L(t)$, the second stage for an accurate estimation of the WBR phase errors is performed to create a full focused image. Unlike $\varphi_L(t), \varphi_R(t)$ requires an exhaustive search time to find a global optimum estimation; therefore, near-optimal estimation techniques are usually employed. Entropy minimization techniques have been proposed for ISAR applications [11, 14]. The SSA [11] is one of effective methods to estimate the WBR phase errors in accurate. However, it requires a considerable amount of computation time when applied to real SAR applications. Therefore, we adopt an iterative golden section search (IGSS) method which requires much less computation time over the SSA. The IGSS method is based on the concept of a golden section search [15] with entropy minimization in the image domain, as with the SSA. The utilization of golden section search for the estimation of phase errors was firstly proposed in [8], which finds optimum coefficients of Legendre polynomials. This paper utilizes the golden section search for direct estimation of all phase errors at every azimuth positions in order to compensate the WBR phase errors in accurate. One factor to consider is that the entropy function in the IGSS method must satisfy the unimodal condition within the search section. Fortunately, when the entire search section is divided into sub-sections, this condition can be satisfied in each sub-section. The final solution will then be obtained by the selection of the best result between two sub-sections with minimum entropy. In our experiment, the condition is satisfied by dividing the entire search section $L: [-\pi,\pi]$ into two the sub-sections of $L^-: [-\pi,0]$ and $L^+: [0,\pi]$, after which a better optimal solution is attainable through GSS iterations. For a clear explanation of our method, definitions of the variables and functions are necessary. After compensation of STV phase error $\varphi_L(t)$, we define $\tilde{g}(t)$, \tilde{g}_n , and ψ_n as follows:

$$\tilde{g}(t) = g(t)e^{-j\varphi_L(t)}
\tilde{g}_n = \tilde{g}(t = t_n)
\psi_n = \varphi_R(t = t_n), \quad n = 0 \sim N_T - 1.$$
(7)

Here, N_T indicates the number of samples of \tilde{g}_n , and ψ_n is the WBR phase error at $t = t_n$. The function of the GSS method is defined as $[\hat{\psi}_p, h_p] = GDN(L, H(\hat{\psi}, \psi_p, \Delta))$, where L indicates the search section, $\hat{\psi}_p$ and h_p are the search result and matching minimum entropy at $t = t_p$, $\hat{\psi}$ is the vector array of $\hat{\psi} = [\hat{\psi}_0 \dots \hat{\psi}_{N_T-1}]$, and Δ is the tolerance parameter of the GSS method. Additionally, the entropy function $H(\hat{\psi}, \psi_p)$ used in our method is defined below similar to the cost function used in [11, 16]

$$H\left(\hat{\psi},\psi_{p}\right) \equiv \sum_{k=0}^{N_{T}-1} \left| \tilde{F}\left(k;\hat{\psi},\psi_{p}\right) \right| \ln\left[\left| \tilde{F}\left(k;\hat{\psi},\psi_{p}\right) \right| \right]$$

$$\tilde{F}\left(k;\hat{\psi},\psi_{p}\right) \equiv \sum_{n=0}^{N_{T}-1} \tilde{f}_{n}e^{-j\frac{2\pi kn}{N_{T}}}$$
where $\tilde{f}_{n} = \tilde{g}_{n} \cdot e^{-j\hat{\psi}_{n}} \quad (n \neq p), \quad \tilde{f}_{p} = \tilde{g}_{p} \cdot e^{j\psi_{p}} \quad (n = p).$

$$(8)$$

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With all of the above definitions, an overall processing flow diagram of the IGSS method is depicted in Figure 2. Here, l and p are the indices of iteration and N_{iter} denotes the maximum iteration number, and ϵ is the threshold for termination. The parameters Δ and ϵ do not need to be fixed but instead can vary with the iterations like $\Delta(l)$ and $\epsilon(l)$ to obtain a better solution.



Figure 2. Processing flow diagram of the IGSS method.



Figure 3. Two extracted range bins and phase errors. (a) Uncorrupted original range bin for target #1. (b) Uncorrupted original range bin for target #2. (c) STV phase error $\varphi_L(t)$. (d) WBR phase error $\varphi_R(t)$.



Figure 4. The estimation result of $\varphi_L(t)$ by the first stage.

4. SIMULATION AND REAL DATA PROCESSING

4.1. Simulations with Point Targets with NNCs

Simulations with point targets were performed to illustrate the performance of the proposed method. We assumed that two extracted range bins contained some NNCs and that the phase error $\varphi(t)$ consisted of both STV and WBR phase errors, as shown in Figure 3.

The result of the first stage is given in Figure 4, which shows that a good approximation of $\varphi_L(t)$ is achieved by the sub-aperture estimation. The final results of the proposed method and other



Figure 5. Simulation results. (a) Blurred image by $\varphi(t)$. (b) Images after compensation of $\varphi_L(t)$. (c) Final compensated images after IGSS. (d) Final compensated images by PGA. (e) Final compensated images by EVM. (f) Final compensated images by WLS. (g) Final compensated images by SSA. (h) Final compensated images by SPA.

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conventional methods are presented in Figure 5. The defocused two images by $\varphi(t)$ are given in Figure 5(a). After compensation of the STV phase errors, focused (but not fully) images are obtained, as shown in Figure 5(b). The final images after second stage with the IGSS method are presented in Figure 5(c), which completely restores the original range bins without any degradation or spurious



Figure 6. The computation time of the IGSS and SSA.



Figure 7. Processing results with a real SAR image. (a) Original image before autofocus, CNT = 6.6. (b) Processed by the PGA, CNT = 6.9. (c) Processed by the SPA, CNT = 14.3. (d) Processed by the SSA, CNT = 46.2. (e) Processed by the proposed method, CNT = 85.5.

targets. In contrast, all other conventional methods which are sensitive to the quality of the extracted range bins show some loss in the amplitude (radar cross section) of each NNCs. Also, many spurious targets appear, as shown in Figure 5(d) for the PGA, 5(e) for the EVM, Figure 5(f) for the WLS, and Figure 5(h) for the SPM. The autofocus techniques such as the PGA and the SPM show that lots of residual phase errors still remain in the processed images as the WBR phase errors are difficult to be estimated using these techniques. To investigate the effectiveness of the first stage in the proposed method, Direct estimation of both $\varphi_L(t)$ and $\varphi_R(t)$ via the SSA was performed. The Figure 5(g) illustrates that the blurring effect of $\varphi_L(t)$ leads to an inaccurate estimation of the total phase error of $\varphi(t)$ and that it should be compensated before the second stage. The computation efficiency of the IGSS was also tested and compared to that of the SSA. The test was performed on a PC equipped with an Intel(R) Xeon X5460 processor, and we measured each processing time for the IGSS and SSA to estimate the WBR phase errors, which were intentionally added to an uncorrupted range bin. Figure 6 shows that the IGSS requires much less computation time than the SSA and that more efficiency is achieved as the length of the range bin increases.

4.2. Experiment with a Real SAR Data

The processing result with a real SAR signal data is given in Figure 7. The resolution is 1 m, and the scene size is $2 \text{ km} \times 2 \text{ km}$ in terms of the range and azimuth. The operation altitude was 10,000 feet, and the weather condition of that day was not good for image acquisition, thus the phase errors of STV and WBR were serious caused by the turbulence of air. The blurring image by the phase errors is shown in Figure 7(a). The processing results of the PGA and the SPA are given in Figures 7(b)and 7(c), which illustrate that the PGA and the SPA enable us to estimate the STV phase errors but that they cannot sufficiently estimate the WBR phase errors, as many random phase errors remain in the processed images. However, the SPA is better than the PGA because some of the WBR phase errors can be approximated with high order Legendre polynomials. The result processing with the SSA is also presented in Figures 7(d), which illustrates that only the SSA method without the first compensation of $\varphi_L(t)$ is not sufficient to provide an accurate estimation of all phase errors $\varphi(t)$, as discussed in the section on point target simulations. The performance of the proposed method is presented in Figure 7(e), which demonstrates that an accurate estimation of both STV and WBR phase errors is achieved such that well focused image is restored without serious degradation. In order to check the performance of each method objectively, an image quality parameter of contrast (CNT = variance/mean) was calculated, and the best value of contrast is obtained by the the proposed method as shown in Figure 7(e).

5. CONCLUSIONS

From the simulations and real SAR image processing assessments, we conclude that the proposed method can provide better performance than several existing autofocus methods in terms of the estimation accuracy and computation time. We illustrate that our method can effectively be applied to the case of low-altitude airborne SAR operations where the WBR phase errors are not trivial.

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