

# Conjoined, 2.4/5-GHz WLAN Two-Monopole System Decoupled Using Mode-Controlled Capacitor for Notebook Computers

Che-Chi Wan and Saou-Wen Su\*

**Abstract**—A low-profile, decoupled two-monopole system with its two parasitic grounded strips conjoined, forming a very compact structure is demonstrated. Each of the two identical antennas comprises a driven coupling strip and a parasitic grounded strip, operating respectively in the 2.4 GHz (2400–2484 MHz) and 5 GHz (5150–5825 MHz) wireless local area network (WLAN) bands. The two parasitic strips are further joined together, becoming a central, grounded T monopole. By loading a capacitor between the T monopole and the antenna ground, the mutual coupling in the 2.4 GHz band can be reduced by about 12 dB. The capacitor in this design is used to control Ant2 monopole mode to cancel out opposite-phased currents of the dipole mode on the T monopole when Ant1 is excited, such that isolation enhancement can be attained. The proposed two-monopole system occupies a compact size of  $5\text{ mm} \times 40\text{ mm}$  (about  $0.04\lambda \times 0.32\lambda$  at 2.4 GHz) and is favorable for applications in the narrow-bezel notebook computers owing to its low profile of 5 mm.

## 1. INTRODUCTION

The demands for higher data rates have increased over a decade. This translates into the requirement of using multiple antennas inside wireless devices to gain more spatial streams in the complex propagation environment. For example, four wireless local area (WLAN) antennas are deployed in the gaming notebook computers to provide more antenna pattern selections for achieving better throughput performance [1]. It is forecasted that future notebook computers will be installed with more than two WLAN antennas for the soon IEEE 11ax communications [2]. For the antenna engineers, this becomes very challenging to further distribute more antenna elements inside the devices because very little space is left for the current notebook computers. For the rationale of limited space, placing two antennas in close proximity (usually less than quarter-wavelength in free space [3]) becomes a feasible solution.

To improve antenna port-to-port isolation, one popular decoupling technique in common practice is to introduce additional coupling path against the original antenna coupling by inserting grounded resonator structures between the antennas as in [4–9]. The decoupling structures include the uses of the meandered strip resonator [4], the T-shaped open slot in the protruded ground [5], the T-shaped decoupling structure [6], the combination of the meandered strip and the T-shaped open slot [7], the same radiator as the decoupling structure [8], and the integrated  $\pi$ -shaped decoupling strip [9]. A different decoupling technique that uses an inductor connecting the open ends of the shorted monopoles is also reported for notebook applications [10]. Another decoupling technique without placing any decoupling structure between antennas is reported as a self-curing technique [11], in which the capacitive load at proper locations on the shorting strips of the inverted-F antennas with the edge-to-edge distance of 9 mm. The most obvious advantage of designing two separate antennas in a two-antenna system is that

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antenna frequency tuning for each coupled antenna can be easily executed. Nevertheless, these above-mentioned papers still show two discrete antenna elements with certain spacing wasted therebetween.

Quite recently, the two couple-fed loops that are joined together without any separation distance between the two antennas are presented in [12]. It is shown that the conjoined section embedded with a capacitor acts like a band-pass structure, which attracts the currents on the ground, when one loop is excited, distributed on this section and not entering the other loop owing its much lower impedance and thereby decouples the antennas. However, the impedance bandwidth covers the single band of the 5G new-radio band (NR) 77 (3300–4200 MHz), and the isolation therein is just better than 12 dB. The antenna height of 6 mm (about  $0.07\lambda$  at 3.3 GHz) is also larger than 5 mm and can not fit in the narrow bezels of recent notebook computers [13–16].

In this paper, we demonstrate a low-profile, conjoined two-monopole antenna system capable of operating in the 2.4/5 GHz WLAN band with isolation better than 19 and 16 dB over the 2.4 and 5 GHz bands and showing a compact size of  $5\text{ mm} \times 40\text{ mm}$  (about  $0.04\lambda \times 0.32\lambda$  at 2.4 GHz). The design comprises two symmetrically identical monopoles, formed by one 5 GHz driven coupling strip and one 2.4 GHz parasitic grounded strip. The parasitic strips are further conjoined, becoming a central, grounded T monopole. By loading a chip capacitor between the T monopole and the antenna ground, the mutual coupling in the 2.4 GHz band can be reduced by about 12 dB (from 7 to 19 dB). Moreover, the two 5 GHz driven strips are inherently decoupled owing to larger distance between them. The capacitor in this study neither function as a band-pass resonant structure as reported in [12] nor is considered as one of the two discrete auxiliary ports in the impedance matrix as calculated in [11]. Substantially different, the capacitor allows the conjoined strips (T monopole) to generate two different resonant modes very close to each other with similar magnitude but out-of-phase surface currents on the parasitic strip of one antenna (Ant2) when the other antenna (Ant1) is excited. Good decoupling between the antennas is thereby attained. A comparison table for the previous work in [4–12] is provided. From Table 1, it can be seen that the proposed design shows a low profile of 5 mm with no separation between antennas and yet offers minimum isolation  $> 16\text{ dB}$  for every band. Details of the design are described, and the results thereof are discussed in the article.

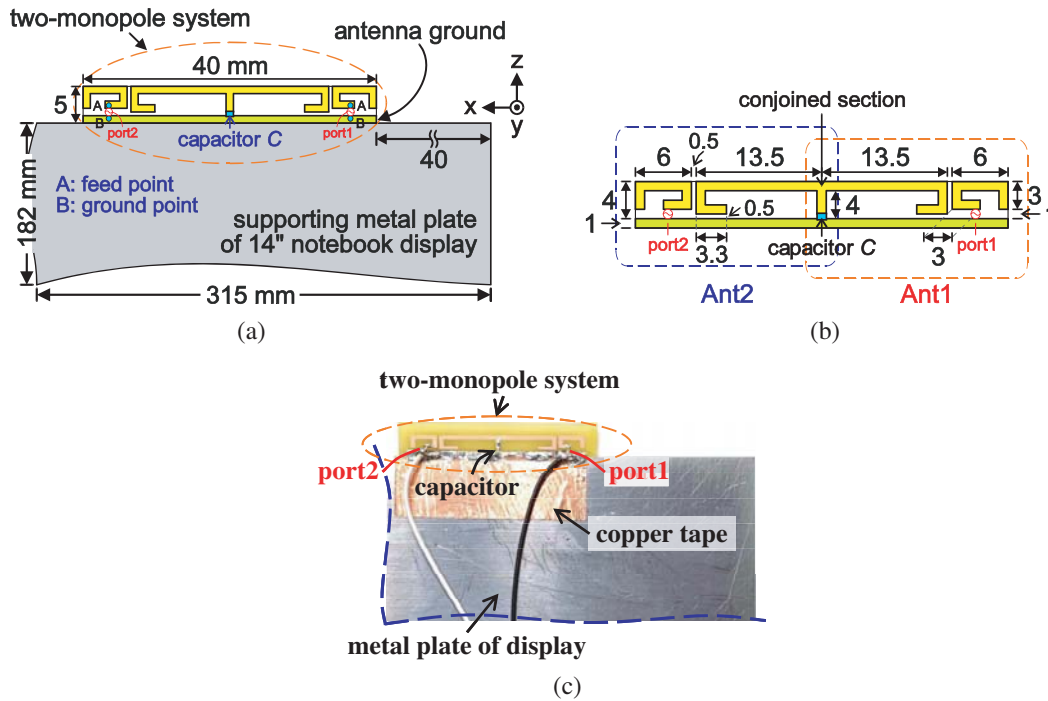
**Table 1.** Comparison of the two-antenna systems [4–12] regarding the operating bands, the overall antenna size, the separation distance between antennas, and the minimum isolation for every band.

Ref.	Operating bands	Size of height $\times$ length	Antenna separation	Isolation*
[4]	2.4/5.2/5.8 GHz	9 mm $\times$ 50 mm	24 mm	18.5 dB
[5]	2.4/5.2/5.8 GHz	9 mm $\times$ 40 mm	26 mm	18 dB
[6]	2.4/5.2/5.8 GHz, 2.5/3.5/5.5 GHz	9 mm $\times$ 54 mm	25.6 mm	15 dB
[7]	2.4/5.2/5.8 GHz	7.5 mm $\times$ 46.4 mm	14.4 mm	15 dB
[8]	2.4/5.2/5.8 GHz	5 mm $\times$ 40 mm	16 mm	15 dB
[9]	2.4/5.2/5.8 GHz	5 mm $\times$ 38 mm	2 mm	16 dB
[10]	2.4/5.2/5.8 GHz	5 mm $\times$ 42 mm	1 mm	17 dB
[11]	2.4 GHz	10 mm $\times$ 43.2 mm	9 mm	16 dB
[12]	3.3–4.2 GHz (5G NR77)	6 mm $\times$ 20 mm	no separation	12 dB
proposed	2.4/5.2/5.8 GHz	5 mm $\times$ 40 mm	no separation	16 dB

## 2. PROPOSED TWO-MONOPOLE SYSTEM

### 2.1. Antenna Configuration and Design Consideration

Figure 1(a) illustrates the proposed two-monopole system affixed to the supporting metal plate of a 14-inch notebook display, measuring  $1\text{ mm} \times 182\text{ mm} \times 315\text{ mm}$ . The metal plate is made of stainless

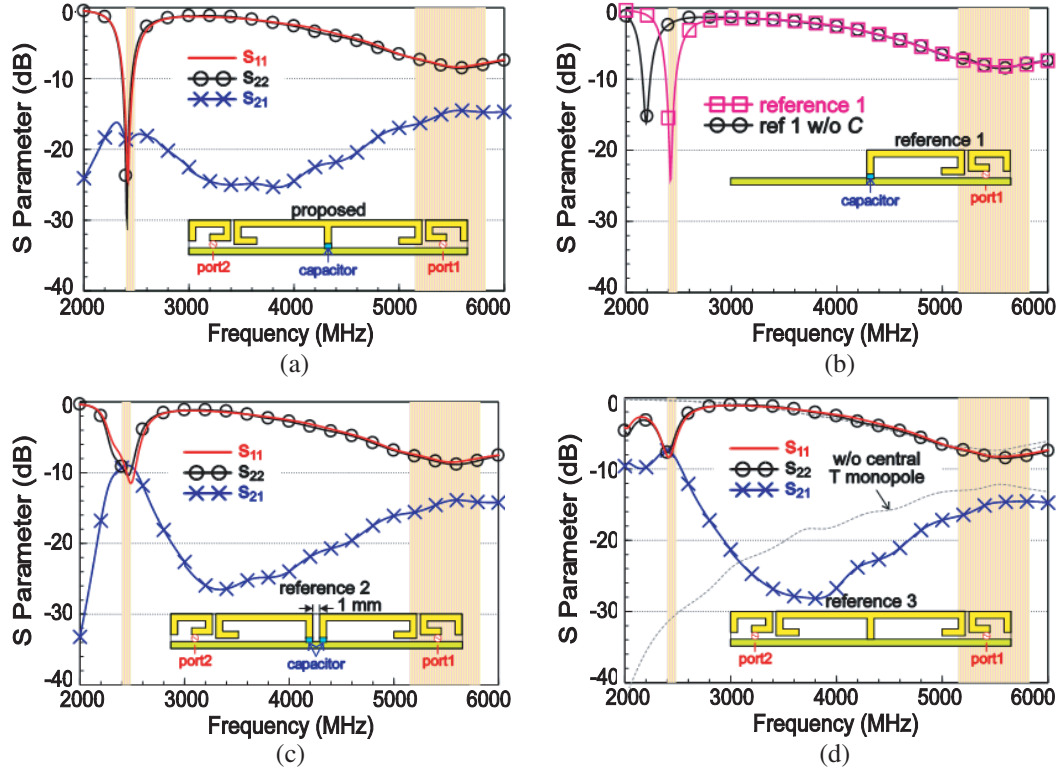


**Figure 1.** (a) Geometry of the conjoined, dual-WLAN-band two-monopole system affixed to the top edge of the supporting metal plate of a 14-inch notebook display. (b) Detailed dimensions of the design prototype. (c) Photo of the fabricated prototype.

plate, coated with the zinc for solderability and can function as the large system ground for both the antennas and the electromagnetic interference (EMI) grounding. The proposed design is fabricated on a 0.4-mm-thick, flame retardant 4 (FR4) substrate ( $\epsilon_r = 4.4$ ) of size 5 mm  $\times$  40 mm only and spaced 40 mm apart from the top-right corner of the metal plate. This 40 mm clearance area is reserved for the mechanical structures, not available for any antenna placement. The small antenna ground of size 1 mm  $\times$  40 mm is also considered in the design footprint as it is required to be connected to the large system ground via small copper tape for practical applications.

The parameters of the preferred design prototype are detailed in Fig. 1(b). The photo of the fabricated prototype is provided in Fig. 1(c). Each monopole antenna (denoted as Ant1 and Ant2) is formed by one driven coupling strip and one parasitic grounded strip. The driven strip is a quarter-wavelength monopole, capable of operating in the 5 GHz WLAN band and at the same time, coupled-feeding the parasitic strip with a small coupling gap of 0.5 mm. Notice that the open end of the driven strip faces away from the parasitic strip, which helps provide better achievable impedance bandwidth for the 5 GHz band. Moreover, the parasitic strip is also a quarter-wavelength resonator, which is designed to generate the lower band for 2.4 GHz operation. Thereby, a dual-band WLAN operation is obtained for single antenna and the proposed design [see Figs. 2(b) and 2(a)]. For ease of studies, all the widths of these strips are kept the same at 1 mm, and the two monopole antennas are symmetrically identical.

The two parasitic strips of Ant1 and Ant2 are further joined together, becoming a central, grounded T monopole. In this case, no separation distance between the two monopoles is required, forming a conjoined two-monopole system with a very small footprint. However, the mutual coupling in the 2.4 GHz band between the monopoles is high, leading to very poor isolation [see Fig. 2(d)]. It is found that by loading a chip capacitor between the grounded T monopole and the antenna ground, the isolation for the 2.4 GHz band can be enhanced. With proper values selected for the capacitor, the monopole mode for Ant2 can be adjusted to be very close to the dipole mode in the central T monopole, which, when Ant1 is excited, creates out-of-phase currents but with similar magnitude on Ant2 and thereby improves the isolation properties. The near-optimum parameters in this paper are simulated by the electromagnetic solver, ANSYS HFSS [17].



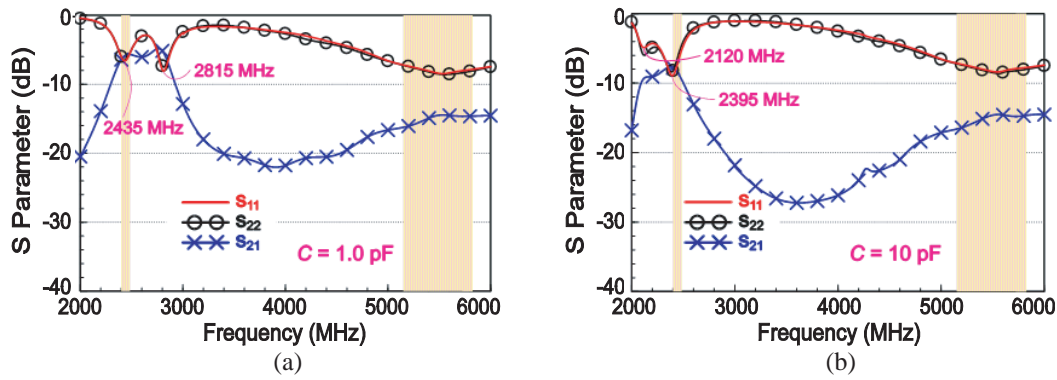
**Figure 2.** Simulated  $S$  parameters ( $S_{11}$  for Ant1,  $S_{22}$  for Ant2,  $S_{21}$  isolation between two antennas) for (a) proposed design, (b) reference case 1 (Ant1, proposed without Ant2), (c) reference case 2 (Ant1 and Ant2 spaced 1 mm apart), and (d) reference case 3 (proposed without capacitor  $C$ );  $C = 2.4$  pF.

## 2.2. Controlling Mechanisms

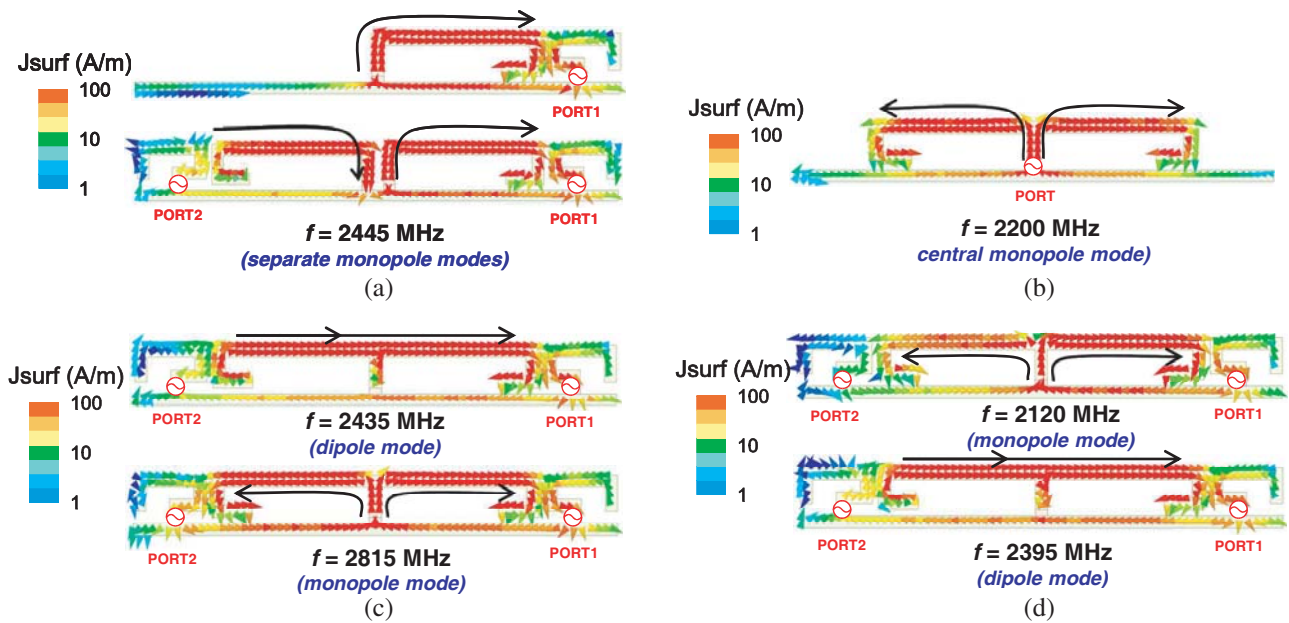
To understand the decoupling mechanisms of the design, several reference cases are analyzed. Fig. 2 shows the simulated  $S$ -parameters for the proposed design, reference case 1 (single monopole), reference case 2 (Ant1 and Ant2 spaced 1 mm apart), and reference case 3 (proposed without capacitor); all the dimensions are kept the same as those shown in Fig. 1. First, for the proposed design, two resonant modes respectively in the 2.4 and 5 GHz bands with isolation ( $S_{21}$ ) better than 18 and 15 dB are generated. For Ant1 only as in reference case 1, the reflection coefficient in Fig. 2(b) is almost the same as those (see  $S_{11}$ ,  $S_{22}$  curves) in Fig. 2(a). This suggests that the achievable impedance bandwidth for the individual antenna is not much affected when the two monopoles are joined together for the proposed design. Notice that the capacitor still has the effect on the antenna frequencies in the lower band (see the black circle curve for reference 1 without  $C$ ) and thus, are reserved for the studies in reference cases 1 and 2. In the case of duplicating Ant1 and symmetrically placing it as Ant2 in close proximity (1 mm gap), the two discrete antennas in Fig. 2(c) have poor isolation at about 9 dB in the 2.4 GHz band, which is caused by strong coupling between the two parasitic strips [see Fig. 4(a)].

As for the proposed design without capacitor (reference 3), it is seen in Fig. 2(d) that even poorer isolation at about 7 dB (17% more energy coupled than the proposed) in the lower band is obtained. These results indicate that grouping the two antennas (Ant1, Ant2) in this design so close that the two separate parasitic strips eventually conjoined can devastate both the input impedance and the isolation properties in the 2.4 GHz band, whereas the  $S$  parameters in the 5 GHz band are comparatively unaffected because the driven coupling strips are inherently decoupled owing to the distance between them (28 mm, about  $0.48\lambda$  at 5.15 GHz). It can be verified by removing conjoined parasitic strips (central T monopole) from the design that the two driven strips produce similar impedance bandwidth in the upper band (no 2.4 GHz operation) with isolation better than 12 dB [see gray dashed lines in Fig. 2(d)].

The capacitor in this design controls the occurrence of the monopole mode for Ant2 to be very close to the dipole mode in the central T monopole. The monopole mode of Ant2 has the opposite-phased currents opposed by those of the dipole mode when Ant1 is excited. As a result of the two resonant modes of almost the same magnitude but with the opposite phases, the mutual coupling can be reduced [18]. The decoupling mechanisms for the design are further elaborated with the aid of Figs. 3 and 4. In Fig. 3, two largely different-scaled values (1.0 vs. 10 pF) of the capacitor are practically selected from the datasheet of Murata GJM series, and two resonant modes can be observed in the 2–3 GHz frequency range. The resonant mode around 2.4 GHz is identified as the dipole mode, formed by the horizontal portions of the two parasitic strips as shown in Figs. 4(c) and (d) and does not move drastically as the values of the capacitor varies. On the other hand, when the capacitor  $C$  increases from 1.0 to 10 pF, the frequencies of the monopole modes for both antennas shift toward the lower frequencies, even below 2.4 GHz [see resonance at 2120 MHz in Fig. 3(b)]. In these cases, the isolation also becomes very poor. Only when these two modes (dipole and monopole) becomes very close to each other can good isolation be attained.



**Figure 3.** Simulated  $S$  parameters for the proposed design in the case of (a)  $C = 1.0$  pF and (b)  $C = 10$  pF.



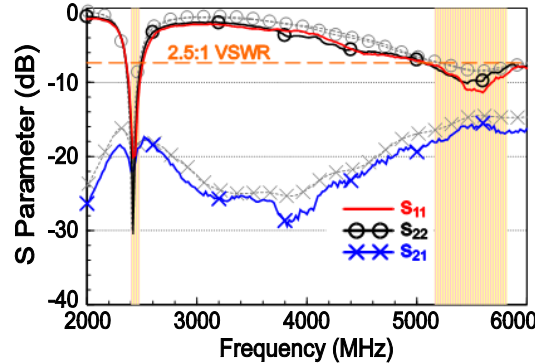
**Figure 4.** Simulated surface currents in the form of vectors at (a) 2445 MHz for reference case 1 and reference case 2, (b) 2200 MHz for central-fed T monopole, (c) 2435 and 2815 MHz for the case of  $C = 1.0$  pF, and (d) 2120 and 2395 MHz for the case of  $C = 10$  pF.

For single monopole (reference 1), it is quite straightforward to see in Fig. 4(a) that at 2445 MHz, the surface current distributions on Ant1 are almost the same as those on Ant1 in reference case 2 while the strongly coupled currents in the opposite phase are seen on Ant2 parasitic strip (also denoted as monopole mode). The surface currents on the horizontal portions of the two parasitic strips flow, in the same direction, through the top portion of the central T monopole when the two parasitic strips are conjoined. This phenomenon results in the dipole mode around 2.4 GHz as seen in Figs. 4(c) and (d). Notice that this dipole mode can only occur when the T monopole is coupling fed by a driven strip. If the signal port is given to the T monopole without any driven strips [see Fig. 4(b)], the surface currents on the T monopole are in the same phase (from the signal to two open ends), resembling the properties of the surface current for the monopole modes in Figs. 4(c) and (d).

Also notice that from the input impedance curves at 2200 MHz where the zero reactance occurs, the resistance for the central monopole mode studied in Fig. 4(d) is very small at about  $8\ \Omega$  (results not shown for brevity). This behavior suggests that for reference case 3 studied in Fig. 2(d), the dipole mode is the dominant resonance and the monopole mode is not responsive. Finally, from these results shown in Figs. 2, 3, and 4, it can be concluded that with the use of the mode-controlled capacitor loaded between the parasitic strip and the antenna ground, isolation enhancement in the 2.4 GHz band can be attained by about 12 dB (from 7 to 19 dB).

### 3. EXPERIMENTAL AND SIMULATION RESULTS

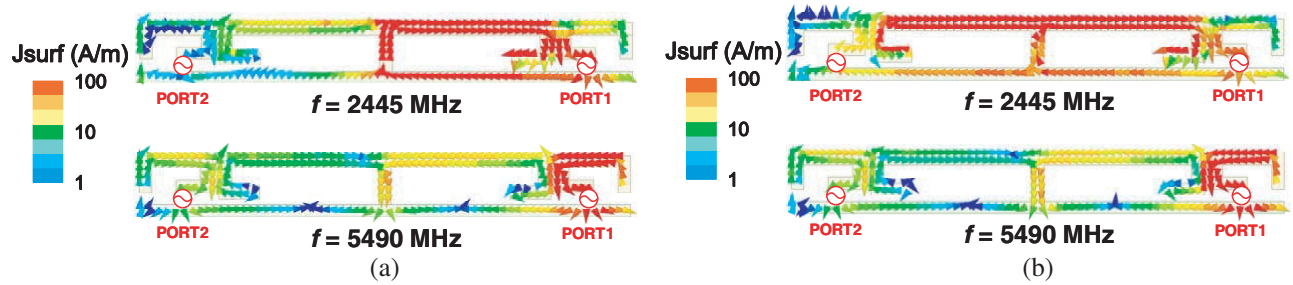
Figure 5 shows the measured and simulated  $S$ -parameters for the proposed two-antenna system. The simulation is presented by gray dashed lines. The targeted 2.4 and 5 GHz WLAN bands are marked by the shaded frequency ranges. The experimental data in general agree with the simulation. The reflection coefficients,  $S_{11}$  and  $S_{22}$ , in the bands of interest are all below  $-7.4$  dB (VSWR of 2.5), which corresponds to about 0.8 dB transmission loss via the antenna and is industrially acceptable for WLAN notebook antennas. The measured isolation ( $S_{21}$ ) between the antennas is better than 19 and 16 dB over the 2.4 and 5 GHz bands. Notice that the 50- $\Omega$  mini-coaxial cables of length about 80 mm were used for feeding the monopoles. The inner conductor of the cable is connected to the feed point (point A) of the monopole while the outer grounding is soldered at the ground point (point B), opposite to the feed point with a feed gap of 1 mm, on the antenna ground. The feed point and the ground point for Ant1 and Ant2 are shown in Fig. 1(a).



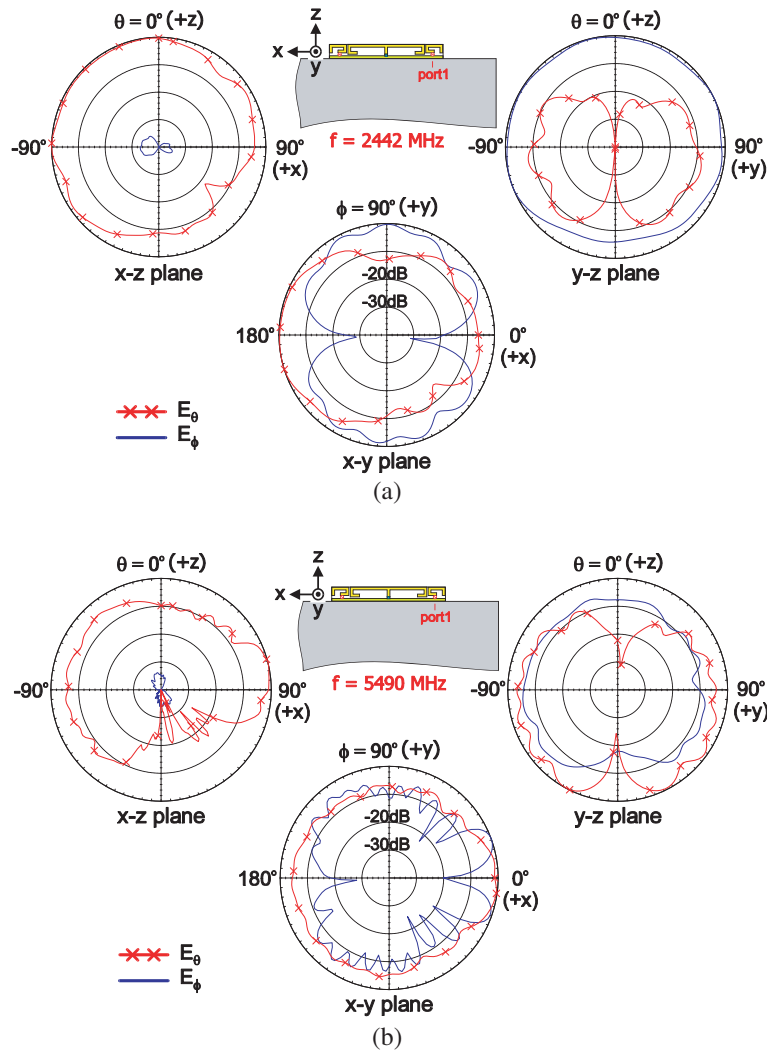
**Figure 5.** Measured and simulated (gray dash lines)  $S$  parameters for the proposed two-monopole system;  $C = 2.4$  pF.

Figure 6 shows the simulated surface-current distributions for Ant1 (port1) excited at 2445 and 5490 MHz for the proposed design with and without (reference 3) the capacitor  $C$ ; the arrows represent the current vectors. First, for port1 excitation at 5490 MHz in the upper band, larger surface currents are seen populated on Ant1 driven strips for both cases with relatively smaller currents induced on the conjoined parasitic strips and Ant2 driven strip. This confirms again that the isolation properties in the 5 GHz band are similar for the proposed and reference case 3 studied in Fig. 2. For the 2.4 GHz lower



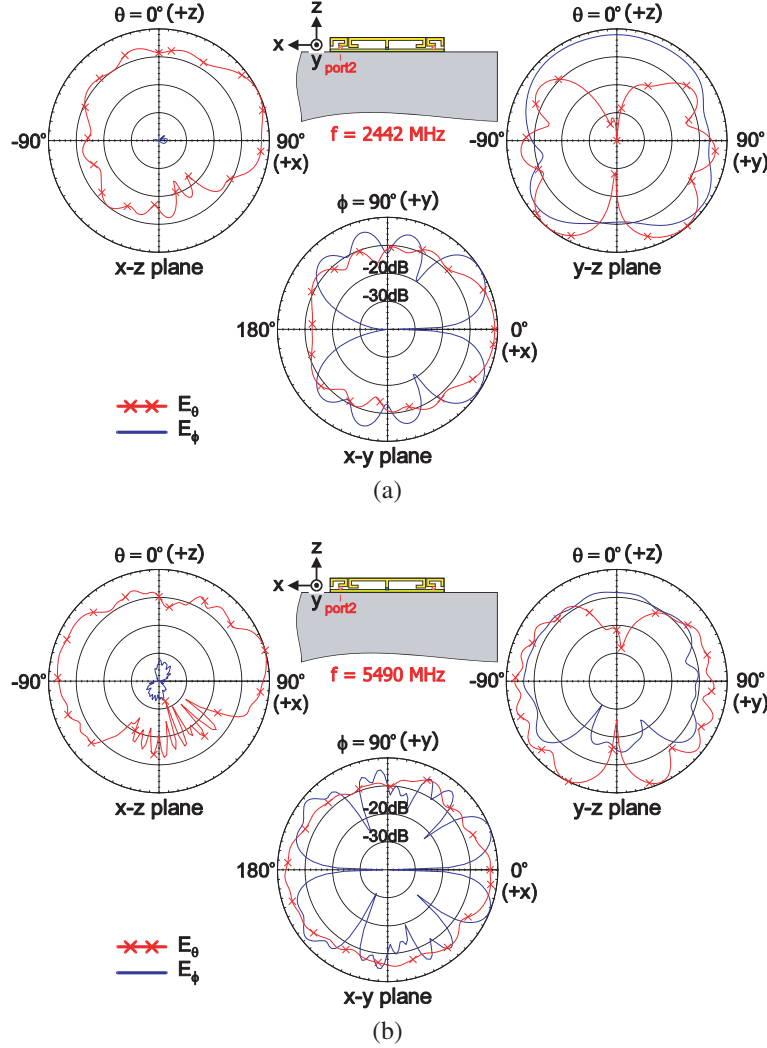


**Figure 6.** Simulated surface currents for Ant1 excited at 2445 and 5490 MHz in the (a) proposed design and (b) reference case 3.



**Figure 7.** Measured 2D radiation patterns of Ant1 in the proposed design at (a) 2442 MHz and (b) 5490 MHz.

band, the currents for the proposed design are mostly distributed on Ant1 parasitic strip (half of the central T monopole), including the image currents on the antenna ground right below Ant1 parasitic strip. However, for the reference case 3, equivalently large currents are found on the conjoined parasitic strips (T monopole) with large image currents entering port2 via the antenna ground, resulting in poorer



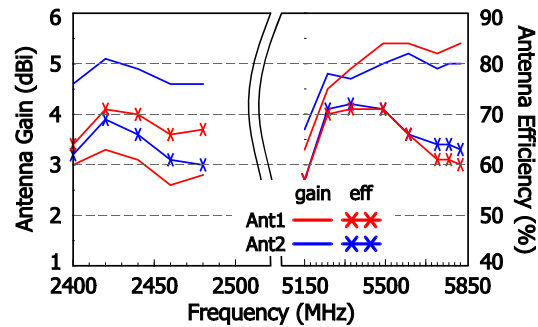
**Figure 8.** Measured 2D radiation patterns of Ant2 in the proposed design at (a) 2442 MHz and (b) 5490 MHz.

isolation in the lower band.

The over-the-air (OTA) performance of the fabricated prototype was measured at our SATIMO chamber of model SG 64, which uses the conical-cut method and has multiple probe arrays [19]. Figs. 7(a), (b) and 8(a), (b) show the measured radiation patterns in  $E_\theta$  and  $E_\phi$  fields for Ant1 and Ant2, respectively, at 2442 and 5490 MHz, the center frequencies of the 2.4 and 5 GHz bands. During the measurement for Ant1 or Ant2, the counterpart Ant2 or Ant1 was terminated at the 50- $\Omega$  load connector. First, comparable  $E_\theta$  and  $E_\phi$  fields are observed in the  $x$ - $y$  planes, which is beneficial for WLAN operation in the complex propagation environment. Second, the radiation patterns in the elevation planes ( $x$ - $z$  and  $y$ - $z$  planes) show larger radiation toward the  $+z$  direction above the display, similar to the radiation characteristics of the WLAN, monopole notebook antenna as studied in [13].

Figure 9 plots the measured, peak antenna gain and antenna efficiency against frequency. For Ant1 in the 2.4 and 5 GHz bands, the peak gain is about 2.9 and 3.3–5.4 dBi with antenna efficiency exceeding 63% and 57% respectively. As for Ant2, the gain is about 4.6 and 3.7–5.2 dBi with efficiency exceeding 58% and 57% in the lower and the upper bands. The larger gain for Ant2 in the 2.4 GHz band, compared with the gain of Ant1, is due largely to larger antenna directivity. From the simulation (not show for brevity), the directivity for Ant2 is larger than Ant1 by about 2 dB at the same frequency and with similar efficiency. The radiation measurement here took account of the antenna mismatch and





**Figure 9.** Measured peak antenna gain and antenna efficiency for Ant1 and Ant2 studied in Figs. 7 and 8.

the cable loss; the realized gain [20] and the antenna efficiency [21] are measured in the chamber. The efficiency was also obtained by calculating the total radiated power of the antenna over the spherical radiation and dividing that total amount by the input power of 0 dBm given to the antenna under test.

#### 4. CONCLUSION

A conjoined two-monopole system suitable for narrow-bezel, notebook applications for dual-band WLAN operation has been proposed. The design comprises two driven coupling strips, one T monopole formed by conjoining two parasitic grounded strips, and one mode-controlled capacitor loaded between the T monopole and the antenna ground, all printed on the substrate of size 5 mm × 40 mm. The driven strips mainly generate the upper band for 5 GHz operation while the parasitic strips are used to excite the 2.4 GHz band. The chip capacitor is introduced to move the monopole mode for one antenna (Ant2) very close to the dipole mode in the T monopole when the other antenna (Ant1) is excited, creating out-of-phase currents but with similar magnitude on Ant2 and thereby improving the isolation properties in the 2.4 GHz band. The measured port isolation is better than 19 and 16 dB over the 2.4 and 5 GHz bands. The antenna efficiency in the 2.4 and 5 GHz bands exceeds 63% and 57% for Ant1 and 58% and 57% for Ant2. The proposed two-monopole system is promising for future multiple notebook antennas for Gbps communications.

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