

Multiwall Carbon Nanotube Impedance Matching Section

Tayfun Günel*

Abstract—In this work, computer-aided impedance analysis and genetic-based synthesis of a multiwall carbon nanotube impedance matching section (MWCNTIMS) are proposed. Transmission line model (TLM) of a multiwall carbon nanotube is used for the computer-aided impedance analysis. Continuous parameter genetic algorithm (CPGA) is used for the genetic-based synthesis. A simple, fast, and effective impedance analysis and synthesis approach for an MWCNTIMS is presented. The results of the analysis and synthesis for different examples of MWCNTIMS are given and discussed in detail. The results show that the effect of variation of the distance from the ground plane of the outer shell is very small on the values of input resistance and input reactance. The values of input resistance and input reactance decrease while the value of inner radius or the total number of shells increases. Since the diameter increases with the increasing value of inner radius and the total number of shells, the values of input resistance and input reactance decrease with increasing diameter. While the value of nanotube length increases, the values of input resistance and input reactance increase.

1. INTRODUCTION

In recent years, a lot of research has been performed on carbon nanotubes (CNTs), their applications, transmission line models of a single wall carbon nanotube (SWCNT) and a multiwall carbon nanotube (MWCNT) [1–12]. CNTs are formed by graphene layers wrapped to cylinders. If they are wrapped as a single layer, it is called SWCNT. If they are wrapped as a multilayer it is called MWCNT. Computer-aided noise analysis of an MWCNT is recently presented in [13]. A simple, fast, and effective impedance analysis and synthesis approach to an MWCNTIMS is proposed in this work. Impedance matching is important for three main reasons [14]. The first reason is that the maximum power is delivered, and power loss in the feed line is minimized. The second reason is the improvement of signal-to-noise ratio of the system by impedance matching receiver components. The third reason is the reduction of amplitude and phase errors by impedance matching in a power distribution network. As far as the author knows, theoretical work does not exist in the literature for the analysis and synthesis of an MWCNTIMS by using the TLM of an MWCNT. In this work, TLM of an MWCNT given in [12] is used for the analysis, and TLM of an MWCNT and CPGA are used for the synthesis. Genetic algorithm (GA) is a global optimization algorithm based on evolution and genetic recombination in nature [15, 16]. In a CPGA, the parameters constituting a chromosome are coded by a single floating-point number. GA and its versions have been extensively used in microwave theory and electromagnetics [17–22]. The other sections of this work are as follows: After the theory is given in Section 2, simulation results are presented and discussed in Section 3. In Section 4, the paper is concluded.

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* Corresponding author: Tayfun Günel (gunelmur@itu.edu.tr).

The author is with the Department of Electronics & Communication Engineering, Istanbul Technical University, Maslak, Istanbul, Turkey.

2. THEORY

The equation for the computation of input impedance of a uniform lossy transmission line terminated in a load impedance ($Z_L = R_L + jX_L$) at a frequency (f) can be given as in [14]

$$Z_{in} = R_{in} + jX_{in} = Z_o \frac{Z_L + Z_o \tanh \gamma L}{Z_o + Z_L \tanh \gamma L} \quad (1)$$

where R_{in} is the input resistance, X_{in} the input reactance, γ the propagation constant, L the length of the line from the load impedance, and Z_o the characteristic impedance of the line. The characteristic impedance of the line is calculated by

$$Z_o = \sqrt{\frac{Z}{Y}} \quad (2)$$

where Z and Y are the per-unit length impedance and per-unit length admittance, respectively. γ is computed from

$$\gamma = \sqrt{ZY} \quad (3)$$

Figure 1(a) shows the cross section of an MWCNT with s shells above the ground plane. Equivalent single conductor model (ESCM) of an MWCNT is represented in Figure 1(b).

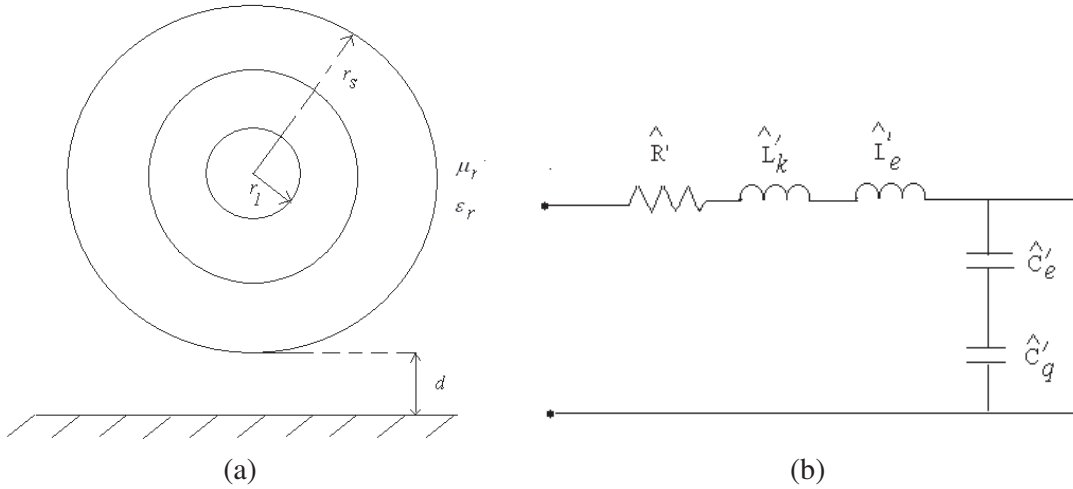


Figure 1. (a) Schematic representation of a MWCNT cross section. (b) Circuit representation of the ESCM of a MWCNT.

Z and Y are computed by

$$Z = \hat{R}' + j\omega \hat{L}' \quad (4)$$

$$Y = j\omega \hat{C}' \quad (5)$$

$\hat{L}'$ and $\hat{C}'$ are given by

$$\hat{L}' = \hat{L}'_k + \hat{L}'_e \quad (6)$$

$$\hat{C}' = \frac{\hat{C}'_e \hat{C}'_q}{\hat{C}'_e + \hat{C}'_q} \quad (7)$$

where $\hat{R}'$ is the equivalent per-unit-length (p.u.l.) quantum resistance; $\hat{L}'_e$ and $\hat{L}'_k$ are the equivalent p.u.l. magnetic and kinetic inductances; $\hat{C}'_q$ and $\hat{C}'_e$ are the equivalent p.u.l. quantum and electrostatic capacitances. $\hat{R}'$, $\hat{L}'_e$, $\hat{L}'_k$, $\hat{C}'_q$, and $\hat{C}'_e$ are computed by the equations given in [12, 13].

The error function for the synthesis of an MWCNTIMS is formed as follows

$$E = \left| R_{in}^c - R_{in}^d \right| + \left| X_{in}^c - X_{in}^d \right| \quad (8)$$

where R_{in}^c , R_{in}^d , X_{in}^c , and X_{in}^d are the computed input resistance, desired input resistance, computed input reactance, and desired input reactance of an MWCNTIMS at a given frequency respectively. The distance from the ground plane of the outer shell (d), the inner radius (r_1), the total number of shells (s), and the nanotube length (L) are selected as unknown values for the synthesis of an MWCNTIMS.

3. SIMULATION RESULTS

Input impedance values of an MWCNTIMS in a frequency range between 0.1 GHz and 100 GHz are calculated by using Eq. (1) for different values of d , r_1 , s , and L . The values of intershell distance, per-unit-length damping resistance, and load impedance are chosen as 0.34 nm, 25.8 k Ω / μ m, and 50 Ω , respectively. It is supposed that the MWCNTIMS is embedded in air.

Figure 2 shows the frequency variation of R_{in} and X_{in} of the MWCNTIMS for different values of d if the values of r_1 , s , L , and Z_L are kept constant ($r_1 = 0.5$ nm, $s = 10$, $L = 0.5$ μ m, $Z_L = 50$ Ω). Change in the values of R_{in} and X_{in} is very small with increasing values of d for a fixed value of Z_L if the other parameters are kept constant.

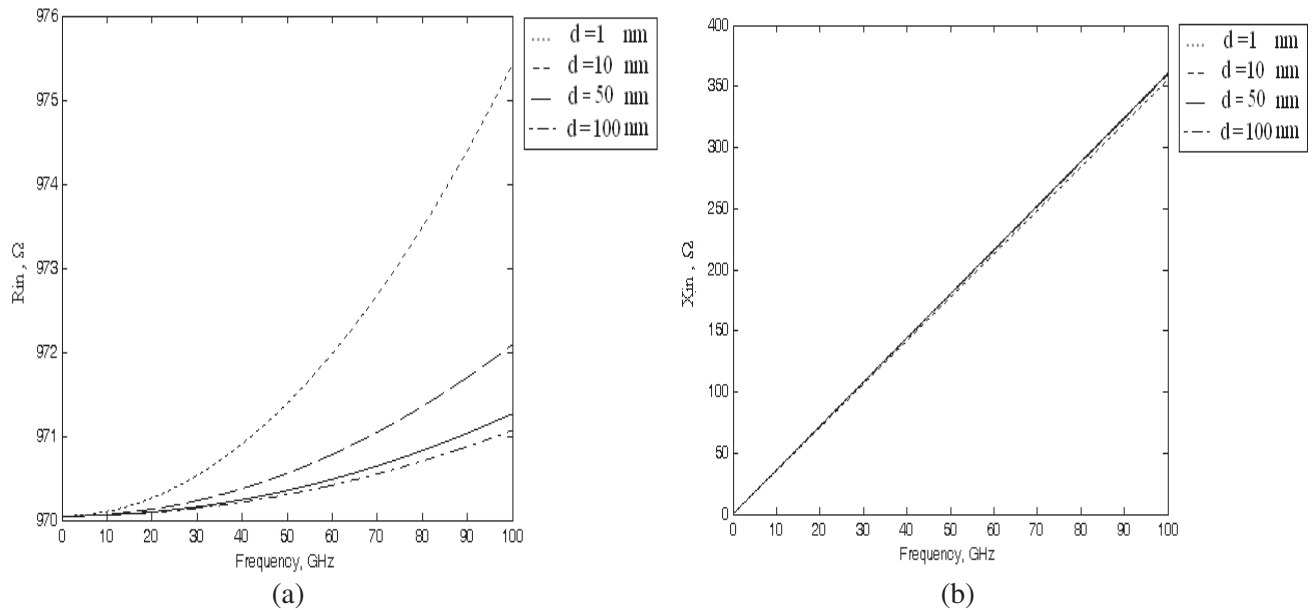


Figure 2. (a) Input resistance. (b) Input reactance of the MWCNTIMS for different values of d .

If the values of d , s , L , and Z_L are kept constant ($d = 1$ nm, $s = 10$, $L = 0.5$ μ m, $Z_L = 50$ Ω), the frequency variation of R_{in} and X_{in} of the MWCNTIMS for different values of r_1 is given in Figure 3. The value of R_{in} decreases from 980 Ω to 140 Ω , and the maximum value of X_{in} at 100 GHz decreases from 355 Ω to 40 Ω with increasing values of r_1 if the other parameters are kept constant.

Figure 4 shows the frequency variation of R_{in} and X_{in} of the MWCNTIMS for different values of s if d , r_1 , L , and Z_L are kept constant ($d = 1$ nm, $r_1 = 0.5$ nm, $L = 0.5$ μ m, $Z_L = 50$ Ω). The value of R_{in} decreases from 980 Ω to 70 Ω , and the maximum value of X_{in} at 100 GHz decreases from 355 Ω to 10 Ω with increasing values of s if the other parameters are kept constant.

If the values of d , r_1 , s , and Z_L are kept constant ($d = 1$ nm, $r_1 = 0.5$ nm, $s = 10$, $Z_L = 50$ Ω), the frequency variation of R_{in} and X_{in} of the MWCNTIMS for different values of L is given in Figure 5. The maximum value of R_{in} at 100 GHz increases from 998 Ω to 4 k Ω , and the maximum value of X_{in}

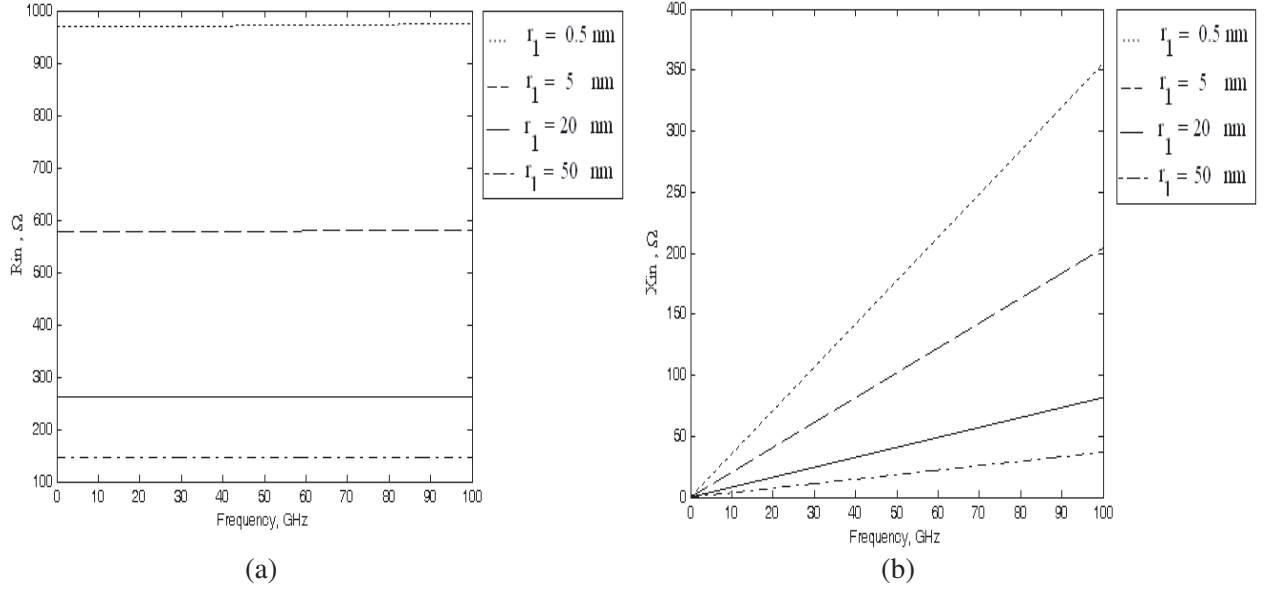


Figure 3. (a) Input resistance. (b) Input reactance of the MWCNTIMS for different values of r_1 .

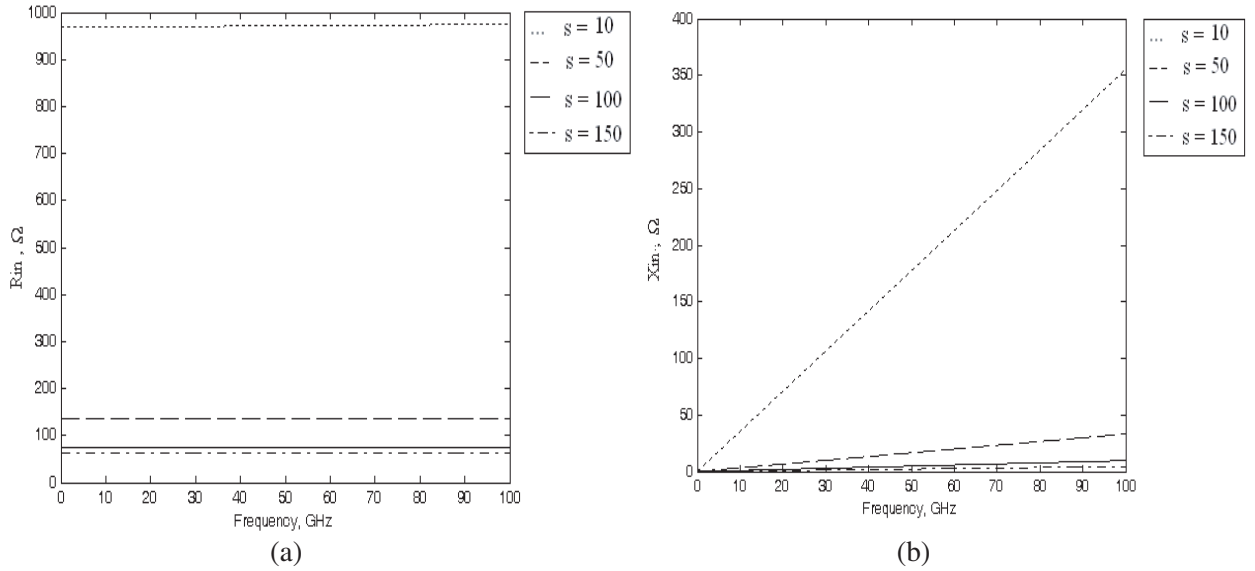


Figure 4. (a) Input resistance. (b) Input reactance of the MWCNTIMS for different values of s .

at 100 GHz increases from 360 Ω to 1020 Ω with increasing values of L if the other parameters are kept constant.

Error function in Eq. (8) is minimized by GPGA to determine the values of d , r_1 , s , and L for the synthesis of an MWCNTIMS. The total number of chromosomes in CPGA is chosen as 1000. The mutation rate is applied as 2%. The iteration number is chosen as 50. The search intervals for the unknown parameters (d , r_1 , s , L) are selected as $0 < d$ (nm) < 100 , $0 < r_1$ (nm) < 100 , $1 < s < 100$, $0 < L$ (μ m) < 100 . The results of the synthesis obtained from the minimization of the error function value by using CPGA for different load and input impedances at different frequencies (f) are given in Table 1. The error function value versus iteration number is shown in Figure 6.

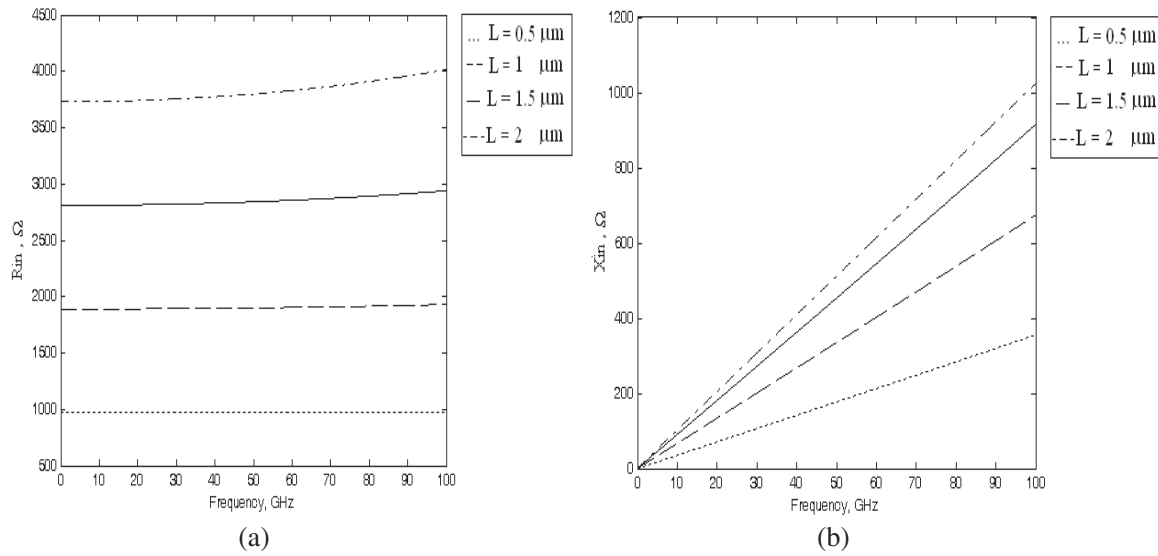


Figure 5. (a) Input resistance. (b) Input reactance of the MWCNTIMS for different values of L .

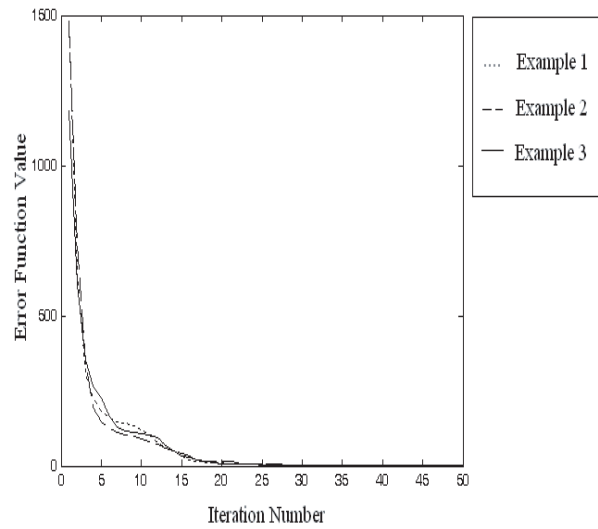


Figure 6. Error function value versus iteration number.

Table 1. The results of the examples for the synthesis of MWCNTIMS.

	Example 1	Example 2	Example 3
d (nm)	1.29	2.39	1.39
r_1 (nm)	89.87	95.51	82.61
s	99	97	98
L (μm)	25.71	17.36	19.45
f (GHz)	50	75	100
$Z_L = R_L + jX_L$ (Ω)	100	$100 + j50$	$100 + j50$
$Z_{in}^d = R_{in}^d + jX_{in}^d$ (Ω)	$300 - j100$	300	$300 + j100$
$Z_{in}^c = R_{in}^c + jX_{in}^c$ (Ω)	$299.99 - j99.91$	$299.96 - j0.005$	$300 + j99.92$
Error (E)	0.1	0.045	0.08

4. CONCLUSION

Computer-aided impedance analysis and genetic-based synthesis of an MWCNTIMS are presented. TLM of an MWCNT is used for the impedance analysis, and TLM and CPGA are used for the synthesis. The results of the analysis and synthesis for different examples of MWCNTIMS are given and discussed in detail. The results show that the effect of variation of the distance from the ground plane of the outer shell on the value of input resistance and reactance is very small. The values of input resistance and input reactance decrease while the value of inner radius or the total number of shells increases. Since the diameter increases with the increasing value of inner radius and the total number of shells, the values of input resistance and input reactance decrease with increasing diameter. While the value of nanotube length increases, the values of input resistance and input reactance increase. The simple, fast, and effective approach presented in this work can be used for impedance analysis and synthesis of different types of impedance matching sections as well as an MWCNTIMS.

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